Using Mid-stage Validation to Increase Confidence in Simulation of TPOs

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DatapointLabs Technical Center for Materials



expert material testing | CAE material parameters | CAE Validation | software & infrastructure for materials | materials knowledge | electronic lab notebooks

Material Testing Expertise

Plastic

Rubber

Film

Metal

Foam

Composite

Cement

Ceramic

Paper

Wire

Fiber

• Product development / R&D support

• CAE-centric

• Commitment to simulation accuracy

• All kinds of materials

• Over 1,800 materials tested each year

• All kinds of material behavior

- Over 200 physical properties:
 - Mechanical properties
 - Thermal properties
 - Flow properties
- Globally available at www.datapointlabs.com visit | browse | buy | download

Tensile Compressive Flexural Stress-strain Poisson's ratio High strain rate Bulk modulus Fatigue Viscoelasticity Stress relaxation Creep Friction Hyperelasticity Thermal expansion Thermal conductivity Specific heat **PVT** Rheology



- Create a process to validate solver+ simulation inputs before reallife application
- Benefits
 - increase confidence
 - reduce risk
 - save time





CAETestBench Validation Mechanism

- Use a standardized geometry
 - May not be real-life part
- Test must be 'perfect'
 - Boundary conditions can be correctly simulated
 - Load case can be correctly simulated
- Comparison
 - Obtain test output that is also available in simulation
 - For example, DIC strain pattern, force v. time...



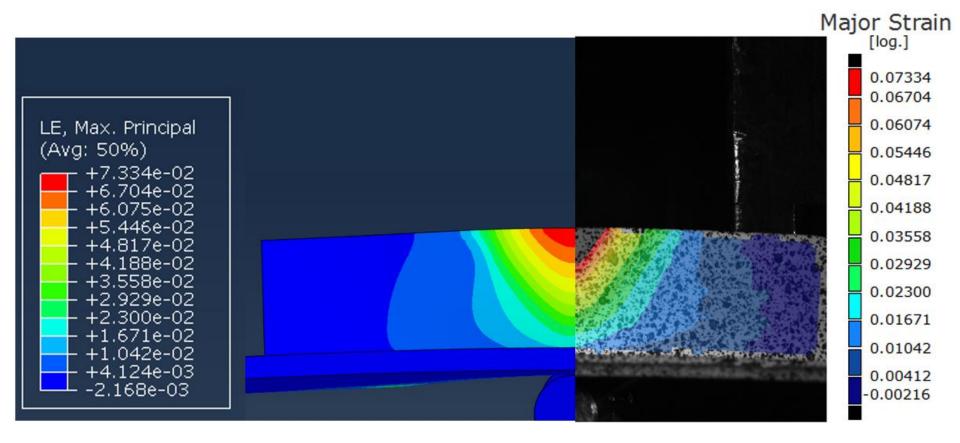
Overview of this Validation

- Measure properties
- Obtain material model parameters
- Perform open loop validation
 - not a test used to create the material model
- Simulate and compare to experiment with DIC
- Quantify simulation accuracy





Case 1: Ribbed Plaque 3 Point Bend



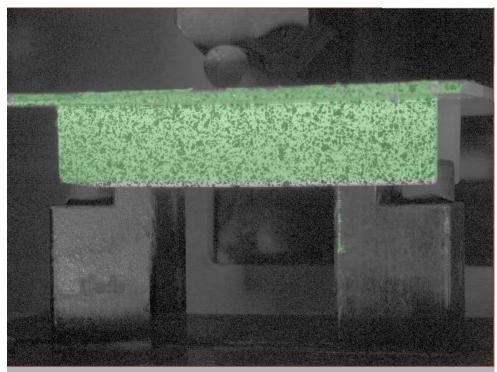






Test Setup

- Instron 8872 universal testing machine (UTM)
- 1 mm/min displacement of nose
- Apply speckle patter to part to allow use of DIC strain capture
- Two camera DIC to capture 3D strain

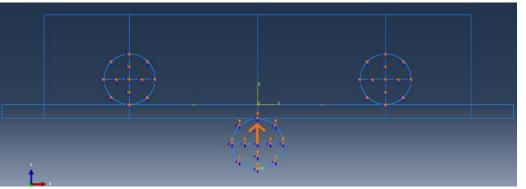






Simulation Setup

- Nose pin:
 - Constrained in all DOF with 2.5mm displaced in Z (Quasi-Static)
- Fixed Support pins
- Part geometry constrained to prevent rigid body movement in the x y direction
- Contact applied in initial step
- Element Formulation: C3D8R (Hex)
- Mesh: 2.25 mm²

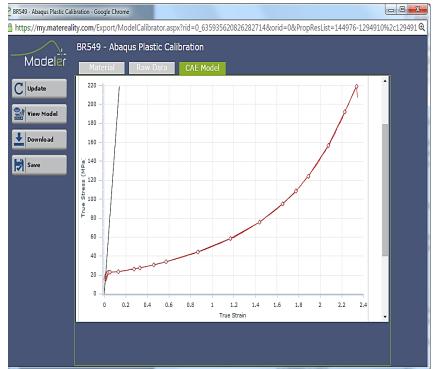


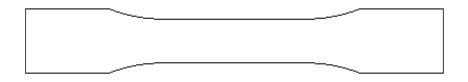




Material Model

- Tensile and Density Tests
- Elastic
 - E = 1572 [MPa]
 - u = 0.29
- Plastic curve (Right)
- Density
 - ρ = 7.9 E-06 [tonne/mm³]
- Measured at QS speeds

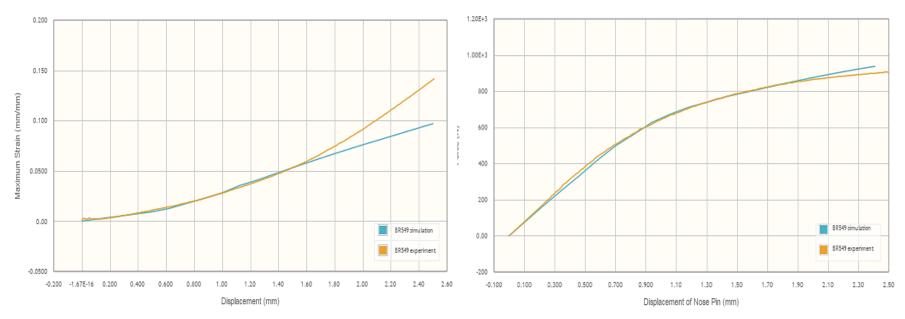








Comparison Simulation to Experiment



•Strain vs. Displacement •Diverges after 2 mm

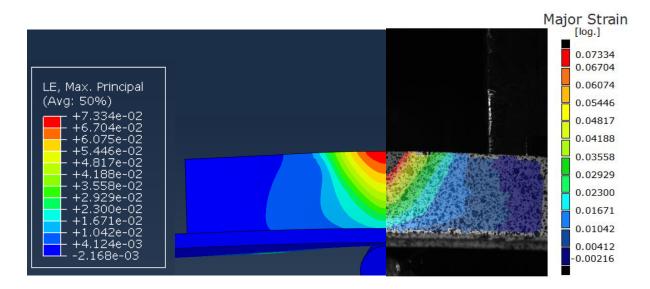
•Force vs. Displacement •Similar response throughout



strengthening the materials core of manufacturing enterprises



Side by Side Comparison of Strains



- Matched the strains in the legend for the DIC image for easy comparison
- The lower strains match closely but the shape of the higher strains on the experiment end up more triangular than the simulation



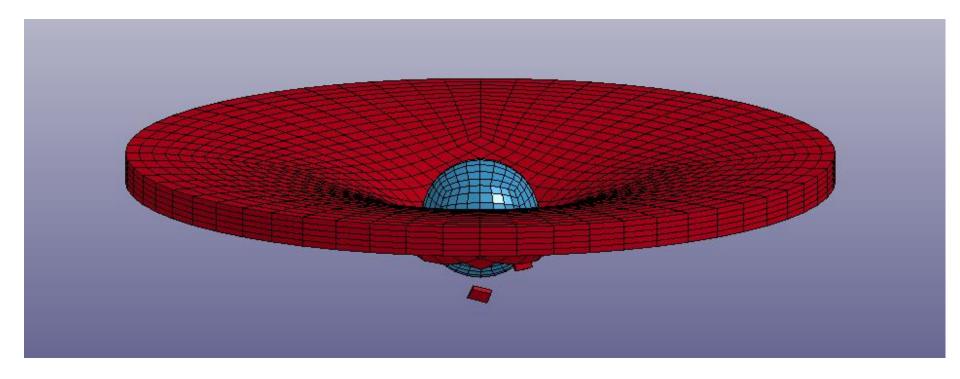


Results

- Abaqus/Explicit models the elasto-plastic behavior of a ductile plastic up to moderate strains when complex modes of deformation are present (complex material model)
- At larger deformations the model deteriorates due to limitations of the elastic-plastic model (Lobo 2006)
- Limits of simulation validity can be applied. Deformations beyond 2 mm may produce inaccurate strain prediction.
- Although strains showed inaccuracy, force values were accurate to higher deformations.



Case 2: Dart Impact







Test Setup

- Dynatup 8250 Impact Tower
- Plate thickness: 3.175 mm
- Clamp Diameter: 76 mm
- Dart diameter:12.7 mm
- Dart weight: 23 kg
- Impact velocity: 3.35m/s

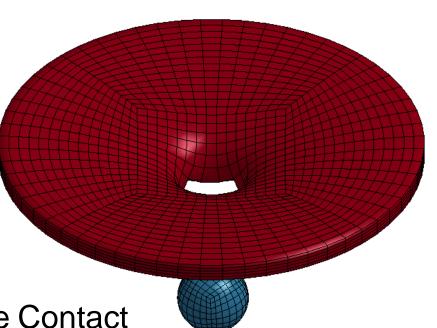






Simulation Setup

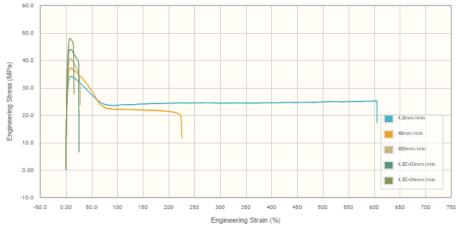
- Plate diameter: 76 mm
- B.C.s: fixed sides
- Impact velocity: 3.35m/s
 - Initial velocity rigid body of dart
- Eroding Surface-to-Surface Contact
- Element formulation: -1 (fully integrates S/R solid)
- Mesh: 3.21mm²





Material Model

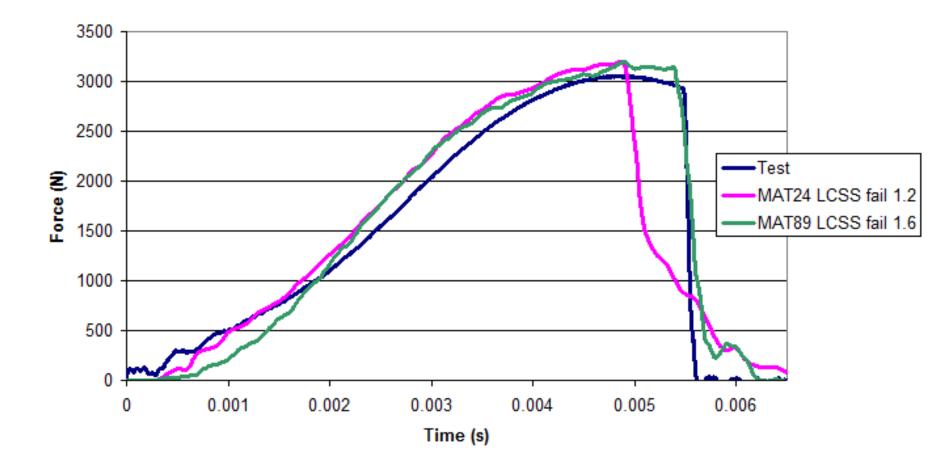
- Tensile and Density Tests
- Elastic
 - E = 2117 [MPa]
 - E = 1664 [MPa] (mat89)
 - v = 0.45
- Density
 - $\rho = 9.09 \text{ E-}10 \text{ [tonne/mm^3]}$
- Strain Rate (0.01/s-100/s)







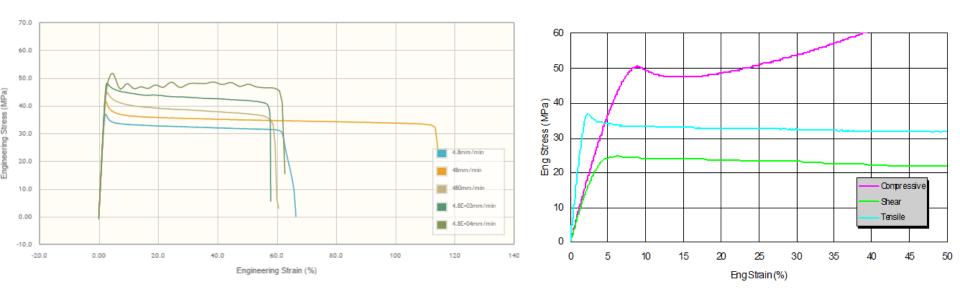
Comparison Simulation to Experiment







Additional Testing for MAT187: ABS

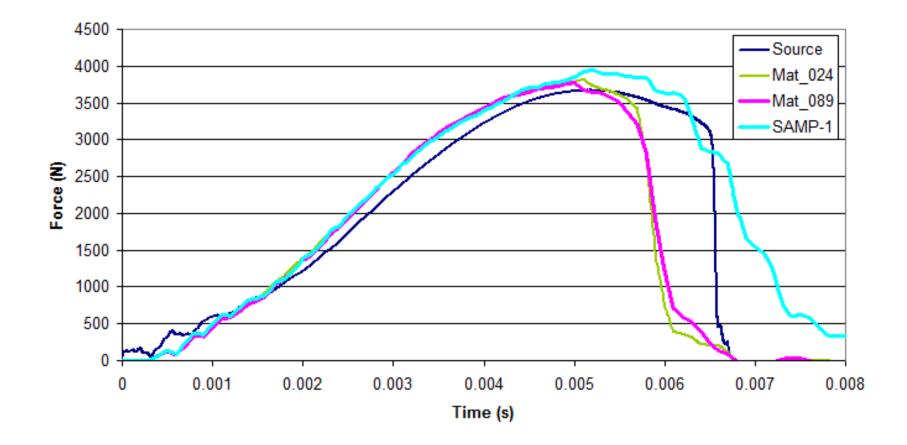


- SAMP-1 allows user to include many different options
 - Post yield Poissons
 - Yield surface
 - Failure based on Triaxiality





Comparison Simulation to Experiment







Results

- MAT_089 performs well in cases where the modulus is not rate-dependent
- MAT_187 modeled the softening behavior prior to failure best
- Measured tensile failure strain cannot be used for FAIL
 - Extrapolation needed to simulate failure
 - Measurements showed that biaxial strain at failure was close to simulation failure strains
 - Without testing the strains for a failure mode, the somewhat arbitrary choice of failure strain seems to be unavoidable with our approach.



Conclusions

- Validation of simulation quantifies the difference between virtual world and reality
- Should be performed each time a material is being tested for use in simulation
- Data, model, and simulation can be checked using test cases that contain real-life behaviors, giving confidence to the analyst



