

# Experimental Calibration and Validation of Radioss Adhesive Laws for Automotive Structural Adhesives

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Applus+ DatapointLabs

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## OVERVIEW OF DATAPOINTLABS

### ■ Experience

- 31 years of experience in materials testing and characterization
  - ISO 17025:2017 accredited, operating on an end-end digital platform
  - Nadcap accredited [Aerospace / Defense] (Metallic/Non-Metallic Materials Testing)

### ■ Operations

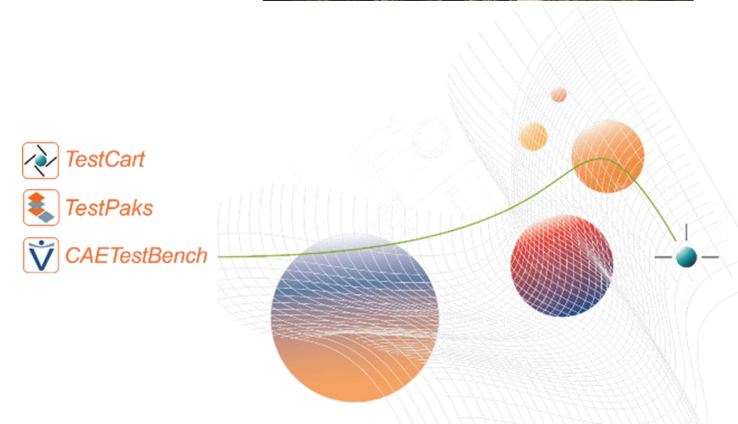
- Testing 2000+ materials per year
- Standard 5-day turnaround
- Comprehensive one-stop testing capability
  - +200 unique tests: all aspects of mechanical, thermal and rheological characterization

### ■ Capabilities

- Materials: plastics, composites, foam, rubber, metals, additive materials, films, adhesives
- May be characterized over a wide range of temperature and environmental conditions



ITHACA, NY  
USA



TestCart

TestPaks

CAETestBench

**Nadcap**  
Administered by PRI

ACCREDITED

Certificate# 17231205927  
Non Metallic Materials Testing


**ISO**  
ISO 17025

**Applus<sup>+</sup>**  
DatapointLabs

**carhs**  
Empowering Engineers

# MOTIVATION AND OBJECTIVES

## Motivation

- Opportunity to bring our testing and simulation expertise into the growing structural adhesives market
  - Increasing use of bonded joints in structural applications
  - Traditional development relies heavily on:
    - Component-level tests
    - Subsystem and system assembly testing
  - High cost and long lead times associated with experimental validation
- 
- Introduction of FEA enables:
    - Early-stage design optimization
    - Reduction in the number of physical tests
    - Decreased dependency on subsystem and system-level tests
  - Faster design iterations and shorter development cycles
  - Improved understanding of failure mechanisms at joint level

## Objectives

- Evaluate the predictive capability of adhesive material laws LAW36 and LAW59
- Development of a robust and transferable methodology for adhesive model calibration across different solvers
- Strengthening internal know-how in fracture-based adhesive testing and modeling

# ADHESIVES MODELS IN RADIOSS

## LAW 36: PLAST\_TAB

- Isotropic elasto-plastic material
- User-defined functions for the work-hardening portion of the stress-strain curve
- Strain-rate dependent
- Easy to implement
- Available for shell and solid elements
- Compatible with multiple failure models

## LAW59 + FAIL: CONNECT

- Anisotropic elasto-plastic material
- User-defined functions for the work-hardening portion of the SS for normal and shear directions
- Strain-rate dependent
- Available only to solid hexahedron elements
- Compatible only with /FAIL/CONNECT
  - Displacement criteria
  - Energy criteria

# EXPERIMENTAL TEST MATRIX



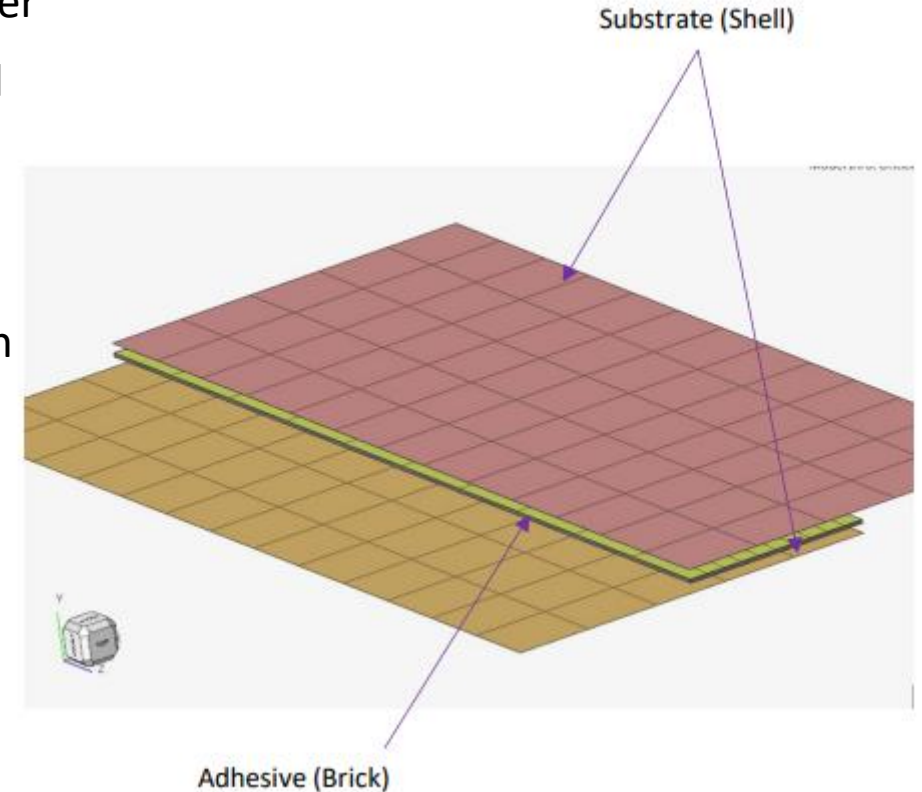
Test Name	Test Geometry	Standard	Material Parameters	Description
Bulk Tensile Test		ISO 527-2	Young Modulus Poisson's Ratio Hardening Curves	Resistance to elastic deformation and transverse contraction in tension
Thick Adherent Shear Test (TAST)		ISO 11003-2	Shear strength Tangential Hardening Curves	Maximum stress in shear
Mode I Fracture Toughness		EN 6033	Mode I Fracture Energy	Resistance to crack propagation (opening mode)
Mode II Fracture Toughness		EN 6033	Mode II Fracture Energy	Resistance to crack propagation (shear mode)

\* All test conditions per performed for 3 Speeds and 3 Thicknesses

# NUMERICAL MODELING APPROACH

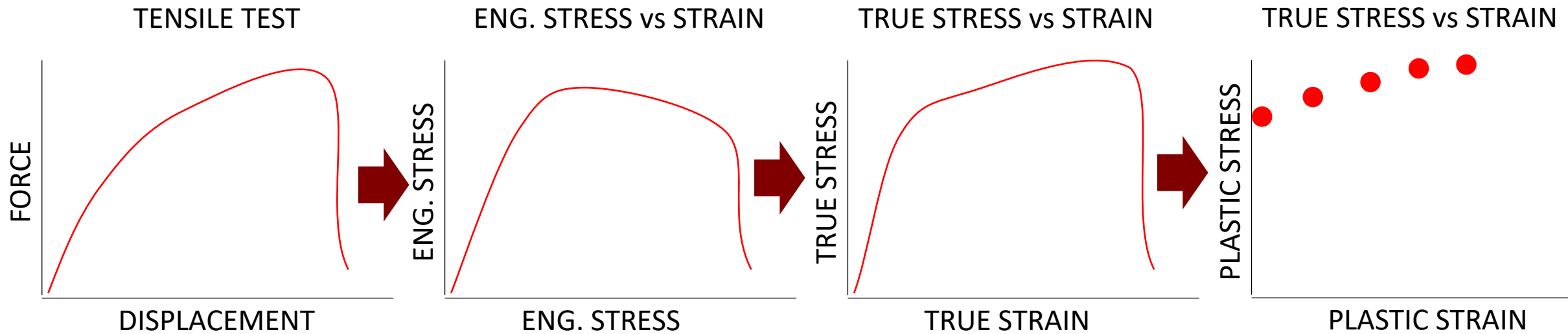
## MODELING STRATEGY AND GLOBAL PARAMETERS

- Finite Element simulations performed using the Radioss explicit solver
- Adhesive layers modeled with 3D solid elements (8 node hexahedral elements TYPE43)
- Metallic substrate modeled with shell elements to reduce computational cost
- Mesh refinement applied in the adhesive layer 2–3 elements through the adhesive thickness
- Coarser mesh in substrates
- Adhesive behavior described using:
  - LAW36
  - LAW59 + FAIL
- TIED Contact between adhesive and substrates
- Displacement-controlled loading used in all simulations
- Quasi-static conditions ensured by low loading rates and energy balance checks



# NUMERICAL MODELING APPROACH

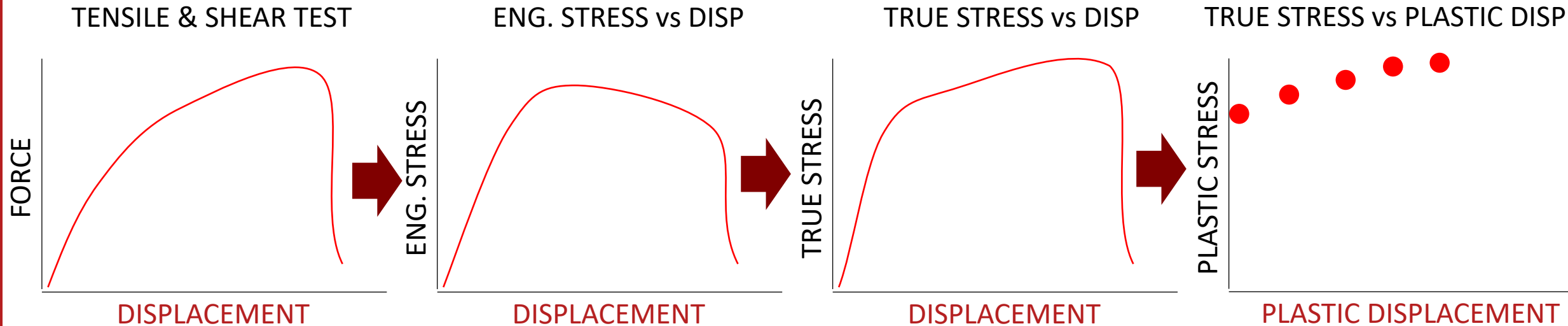
## LAW36: Elasto-plastic tabular model



- Elastic parameters from the highest strain-rate curve
- Power law fitting when possible
- Extrapolation beyond min. and max. strain-rates
- Strain-rate filtering activated

# NUMERICAL MODELING APPROACH

## LAW36: Elasto-plastic tabular model



- Elastic parameters are per unit of length (Preferable to add a Butt Joint Tensile test to obtain these data)
- Icomp flag set to 0: symmetrical elasto-plastic behavior in compression
- Strain-rate filtering activated

# NUMERICAL MODELING APPROACH

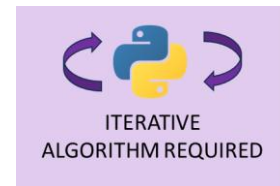
## LAW 59 Failure model

- Multidirectional failure (coupled failure formulation)
- Calibration of both criteria:
  - Displacement criteria

$$\underbrace{\left| \frac{\bar{u}_N}{\bar{u}_{\max N}} \cdot \alpha_N \cdot f_N(\dot{u}_N) \right|^{\text{exp}_N}}_{\text{TENSILE TEST}} + \underbrace{\left| \frac{\bar{u}_T}{\bar{u}_{\max T}} \cdot \alpha_T \cdot f_T(\dot{u}_T) \right|^{\text{exp}_T}}_{\text{SHEAR TEST}} > 1 \quad (1)$$

- Energy criteria

$$\underbrace{\left( \frac{En}{EN_{\max}} \right)^{N_n}}_{\text{TENSILE TEST}} + \underbrace{\left( \frac{Et}{ET_{\max}} \right)^{N_t}}_{\text{SHEAR TEST}} > 1 \quad (2)$$

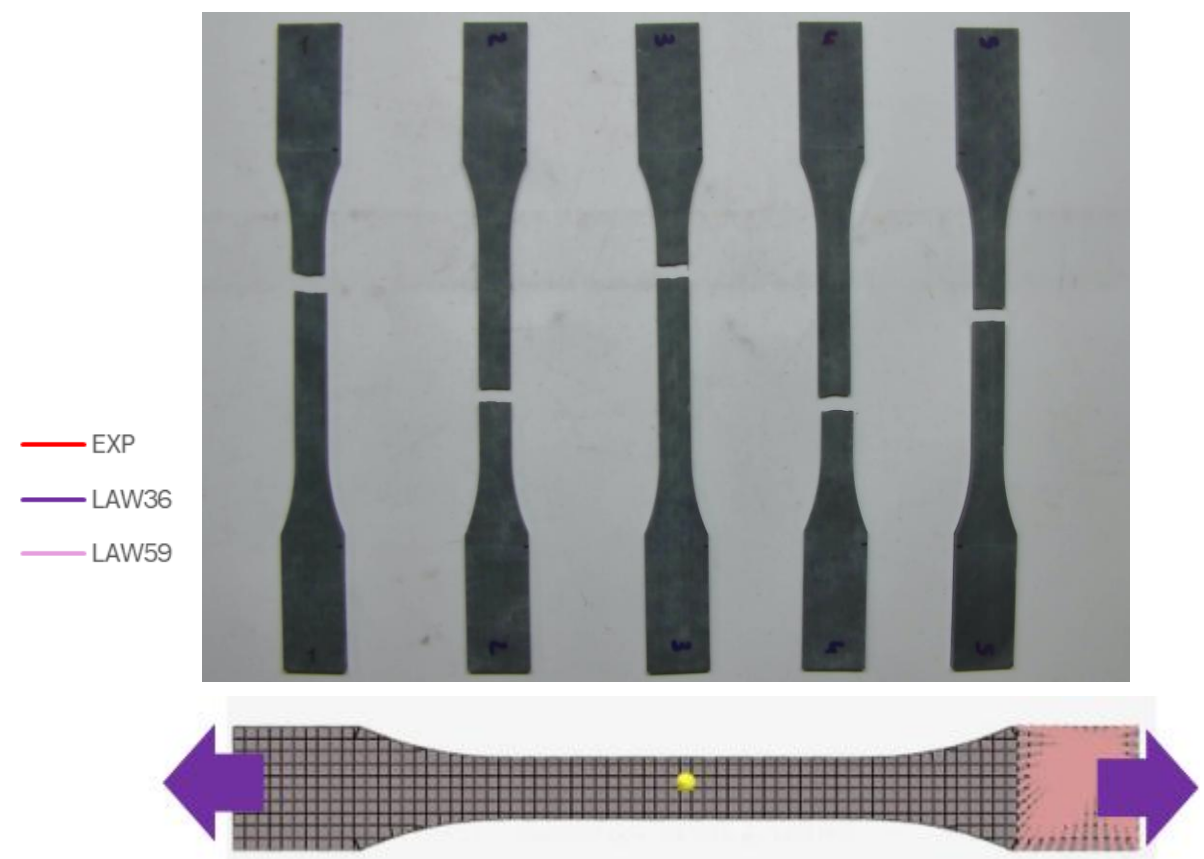
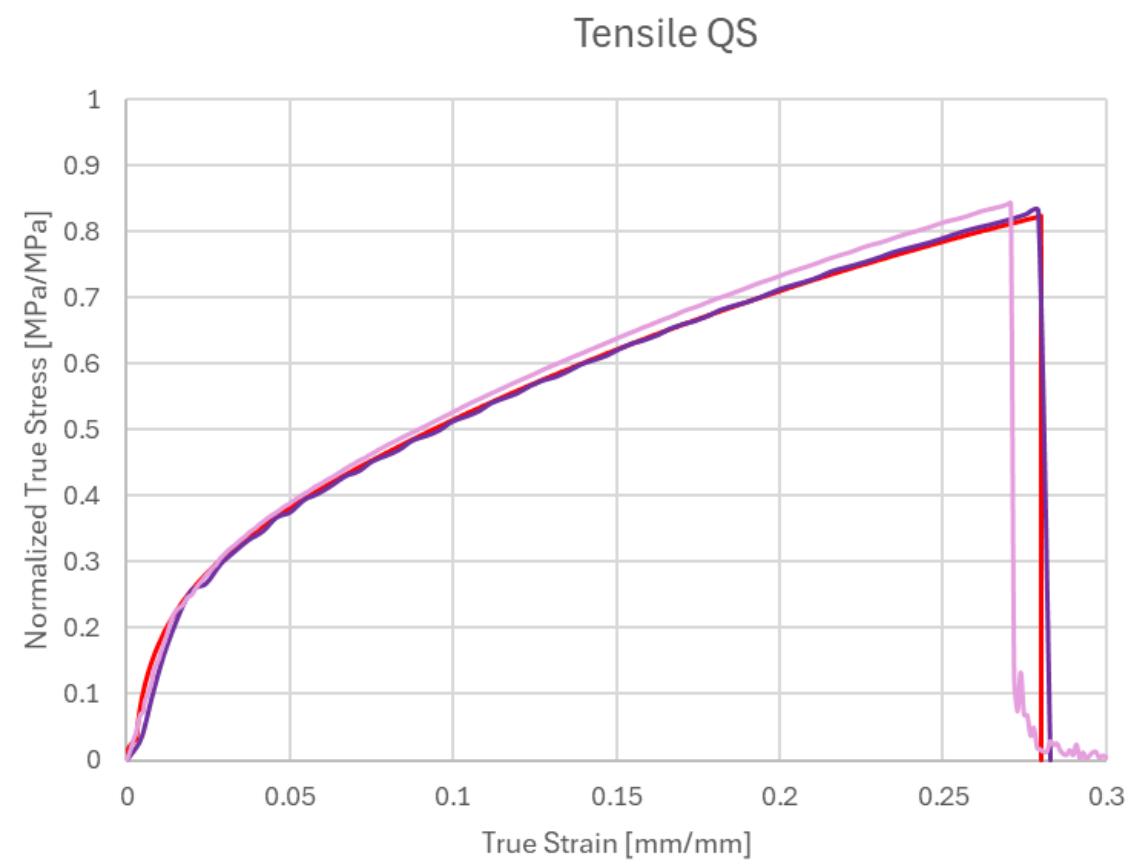


- Softening

$$\sigma = \sigma \left( 1 - \frac{D}{T_{\max}} \right)^{N_{\text{soft}}} \quad (3)$$

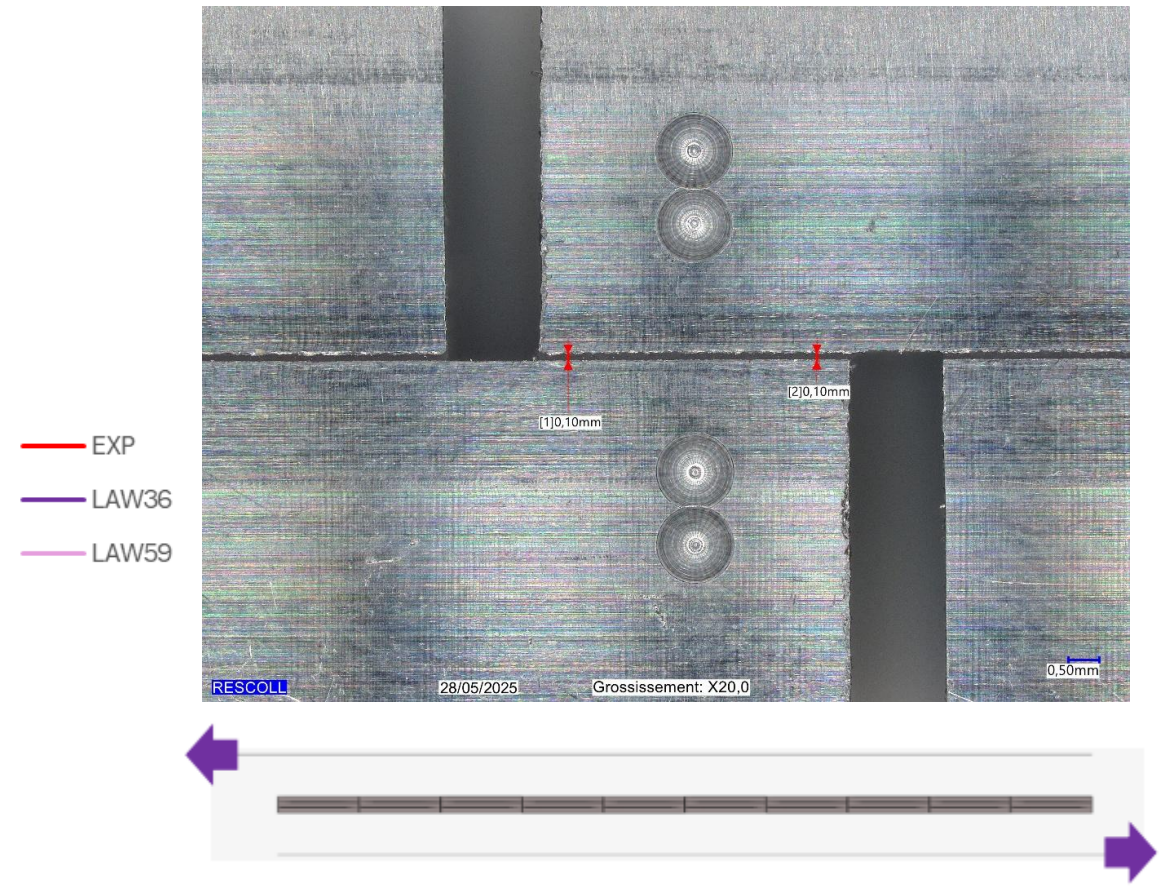
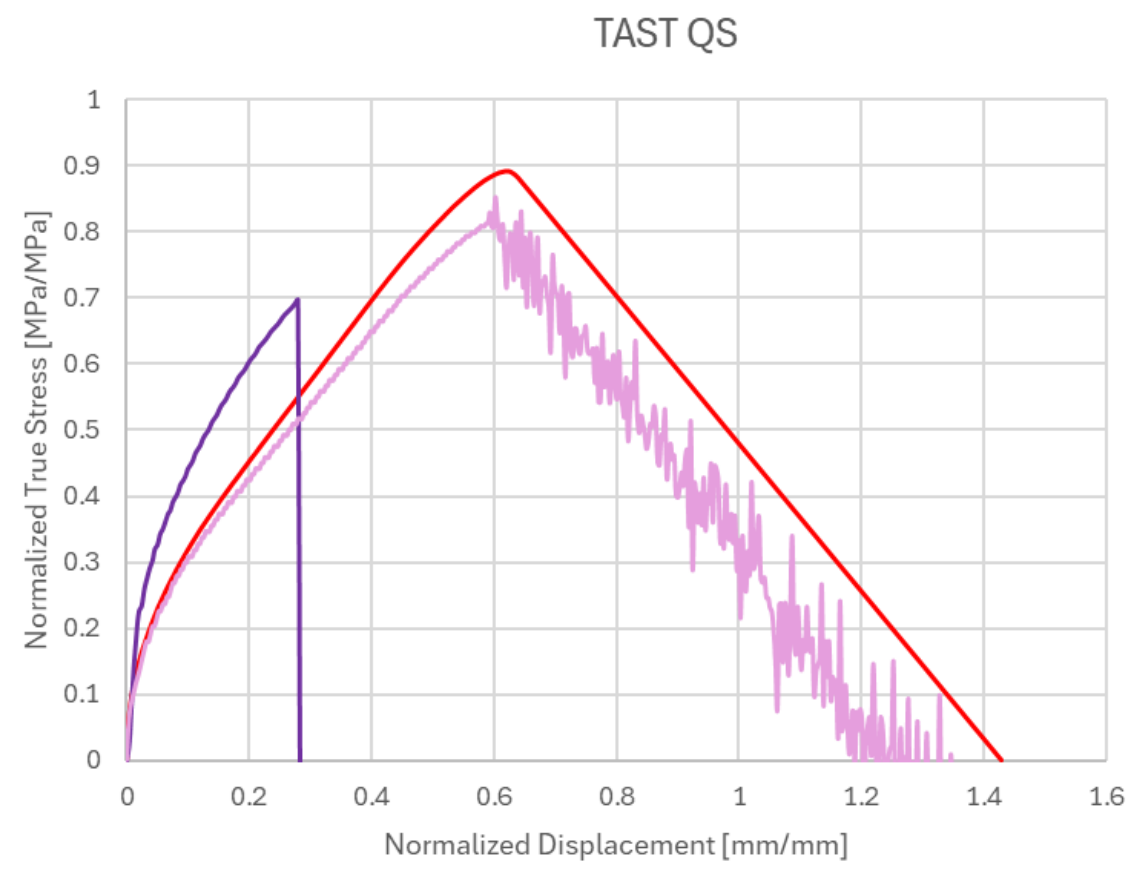
# RESULTS

## Bulk Tensile Test



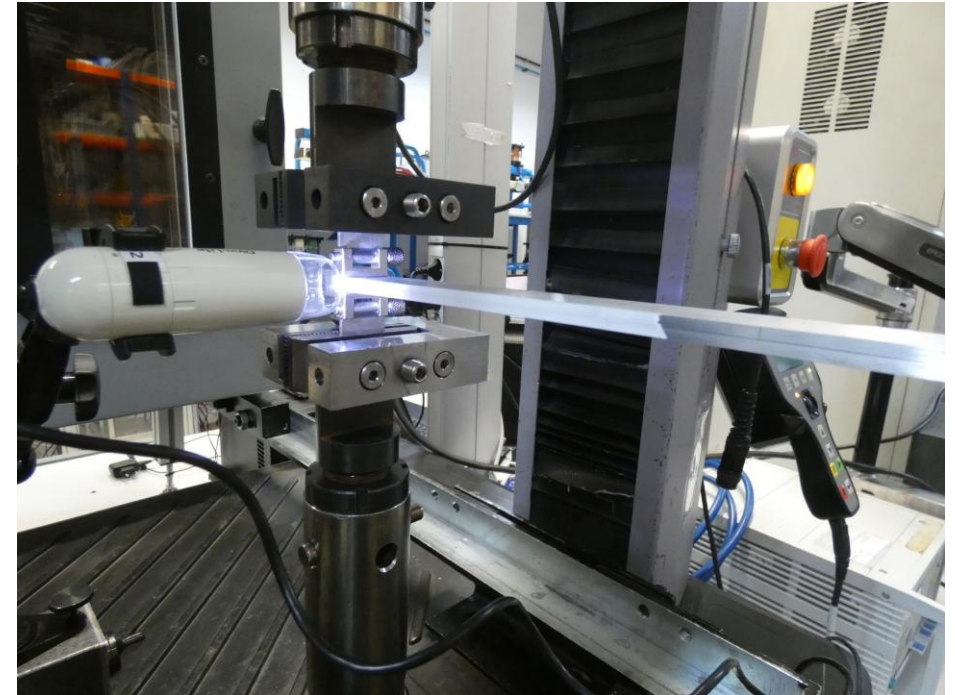
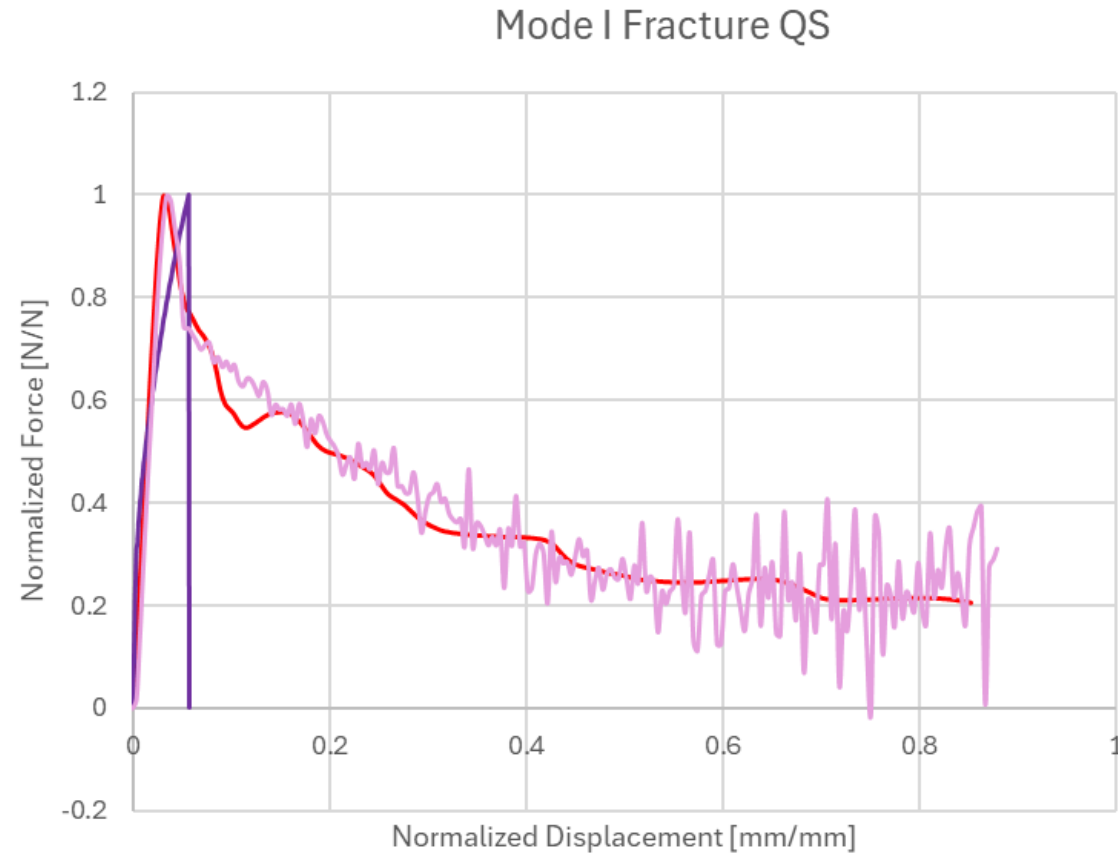
# RESULTS

## Thick Adherent Shear Test

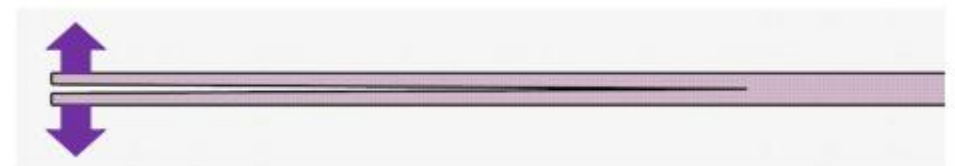


# RESULTS

## Mode I Fracture Toughness



— EXP  
 — LAW36  
 — LAW59



# DISCUSSIONS: Comparative Assessment



## Correlation with Tests

- **Tensile test**
  - Both models reproduce peak load accurately
  - Similar stiffness response
- **TAST**
  - LAW36 slightly overpredicts peak load
  - LAW59 shows better agreement in post-peak response
- **Mode I Fracture**
  - LAW36 fails to reproduce measured fracture energy
  - LAW59 accurately matches G1c and crack growth behavior

## Failure Prediction

- **LAW36**
  - Damage initiation well captured
  - Failure tends to be abrupt and localized
  - Limited capability to reproduce progressive crack growth
- **LAW59**
  - Accurate damage initiation and evolution
  - Progressive degradation observed in all loading modes
  - Realistic crack initiation and propagation in Mode I tests

# DISCUSSIONS: Comparative Assessment



## Predictive Capabilities

Test Condition	Law 36	Law 59
Tensile Response	Robust	Robust
Shear Response	Acceptable	Robust
Mode I Fracture	Limited	Robust

## Calibration Effort

Criterion	Law 36	Law 59
Calibration Effort	Low	High
Numerical stability	High	Moderate
Mesh sensitivity	Low	High
Computational cost	Low	Moderate

# DISCUSSIONS: Comparative Assessment



## Summary

- **Law 36**
  - Efficient and robust for strength-driven applications
  - Suitable for preliminary design and global assessments
- **Law 59**
  - Physically consistent fracture representation
  - Superior for joint-level simulations and failure analysis
  - Preferred when crack propagation and energy dissipation are critical

## NEXT STEPS

### Roadmap 2026

#### 1. Adhesive model + Rigid substrate + Tied connection

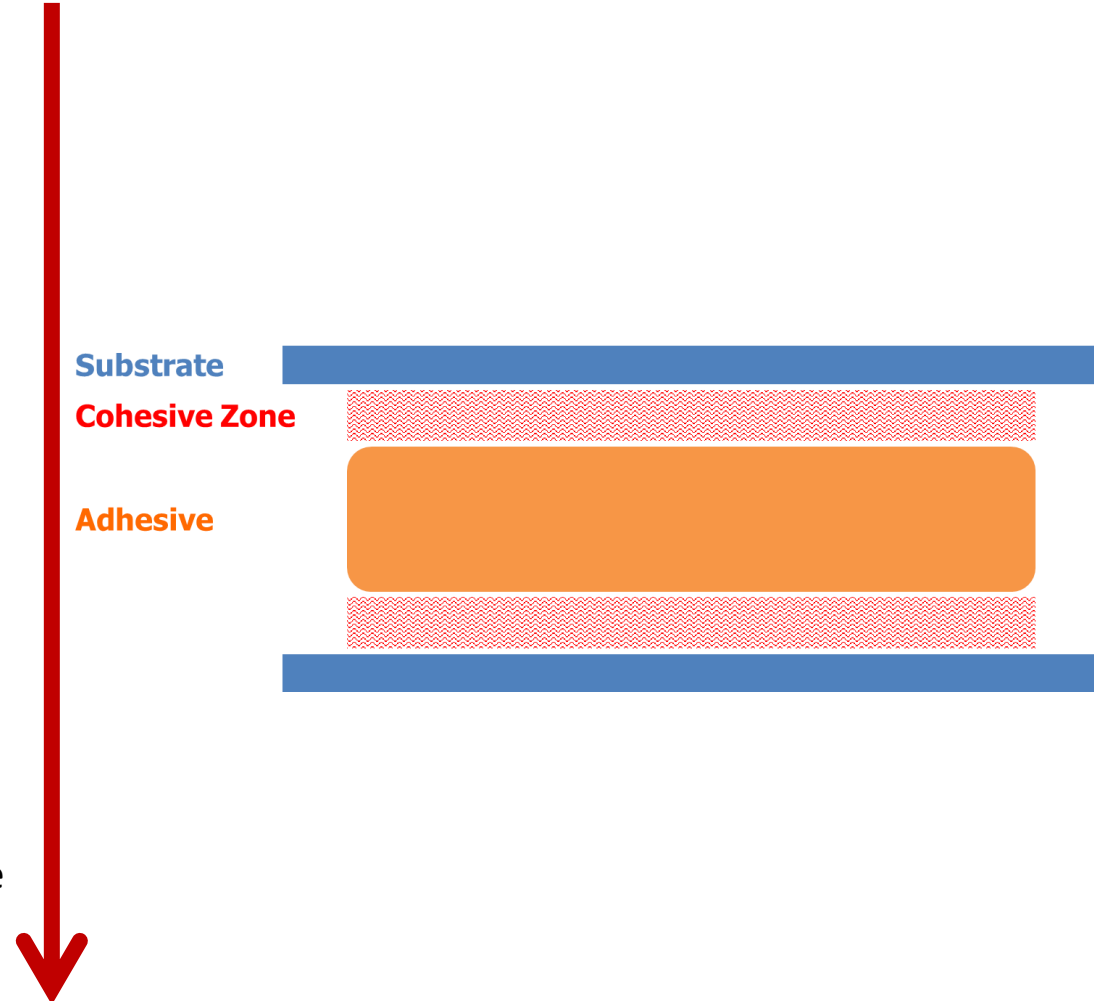
- Simple to calibrate
- Good accuracy of the adhesive behavior
- Failure within the adhesive

#### 2. Adhesive model + Substrate model + Tied connection

- More complex to calibrate
- More testing needed
- Better accuracy on the prediction of the union behavior
- Failure within the adhesive or the substrate

#### 3. Adhesive model + Substrate model + Cohesive zone model

- More complex to calibrate
- Best accuracy on the prediction of the union behavior
- Failure within the adhesive, the substrate or the cohesive zone





# Thank You!

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