



Perspective- Material Modeling and Mold Analysis

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A look back

- Advent of simulation- early successes
- Melt-solid transitions- the case for a unified material model
- Post-fill- PVT and the prediction of shrinkage
- Viscous heating- impact on flow behavior, degradation
- Why CRIMS has to work so hard

Advent- pre 1990

- Solid scientific study into rheology (Hieber et al)
- Very strong rheological models
- Relatively simple simulation-fill patterns
 - u Modest effect of phase change
 - u Rheology, thermal property controlled behavior

$$\eta = \frac{\eta_0}{1 + \left(\frac{\eta_0 \dot{\gamma}}{\tau^*} \right)^{(1-N)}}$$

$$\eta_0 = D_1 \exp \left[\frac{-A_1 (T - T^*)}{A_2 + (T - T^*)} \right]$$

$$T^* = D_2 + D_3 P$$

η Viscosity (Pa.sec)

$\dot{\gamma}$ Shear Rate (sec⁻¹)

T Temperature (C)

P Pressure (Pa)

Unknowns : $D_1 D_2 D_3 A_1 A_2 \tau^* N$

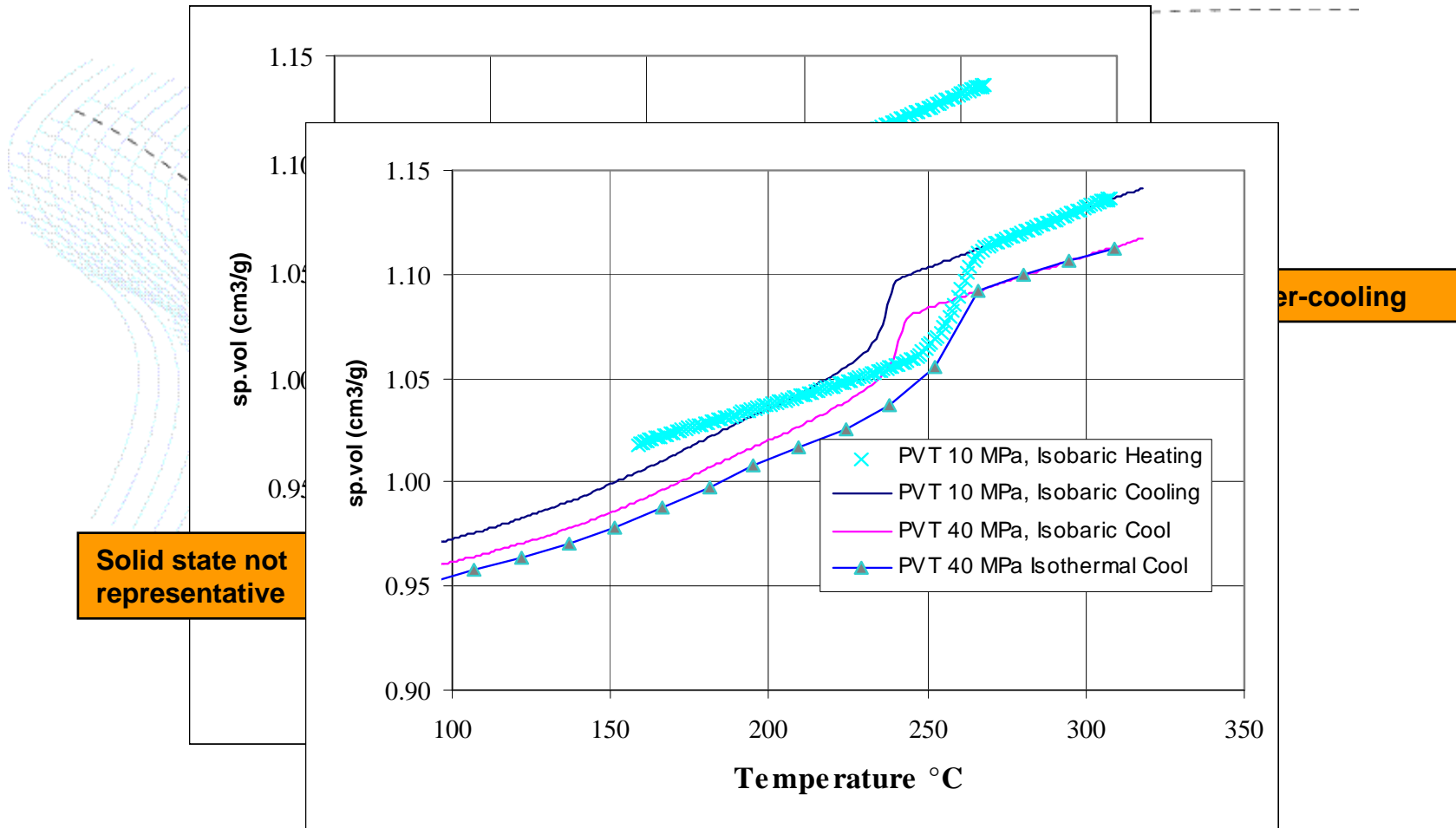
Post-Filling Challenges

- Simulation highly sensitive to very slightly varying property behavior (PVT)
 - u Location/nature of transition
 - u Absolute values of PVT properties

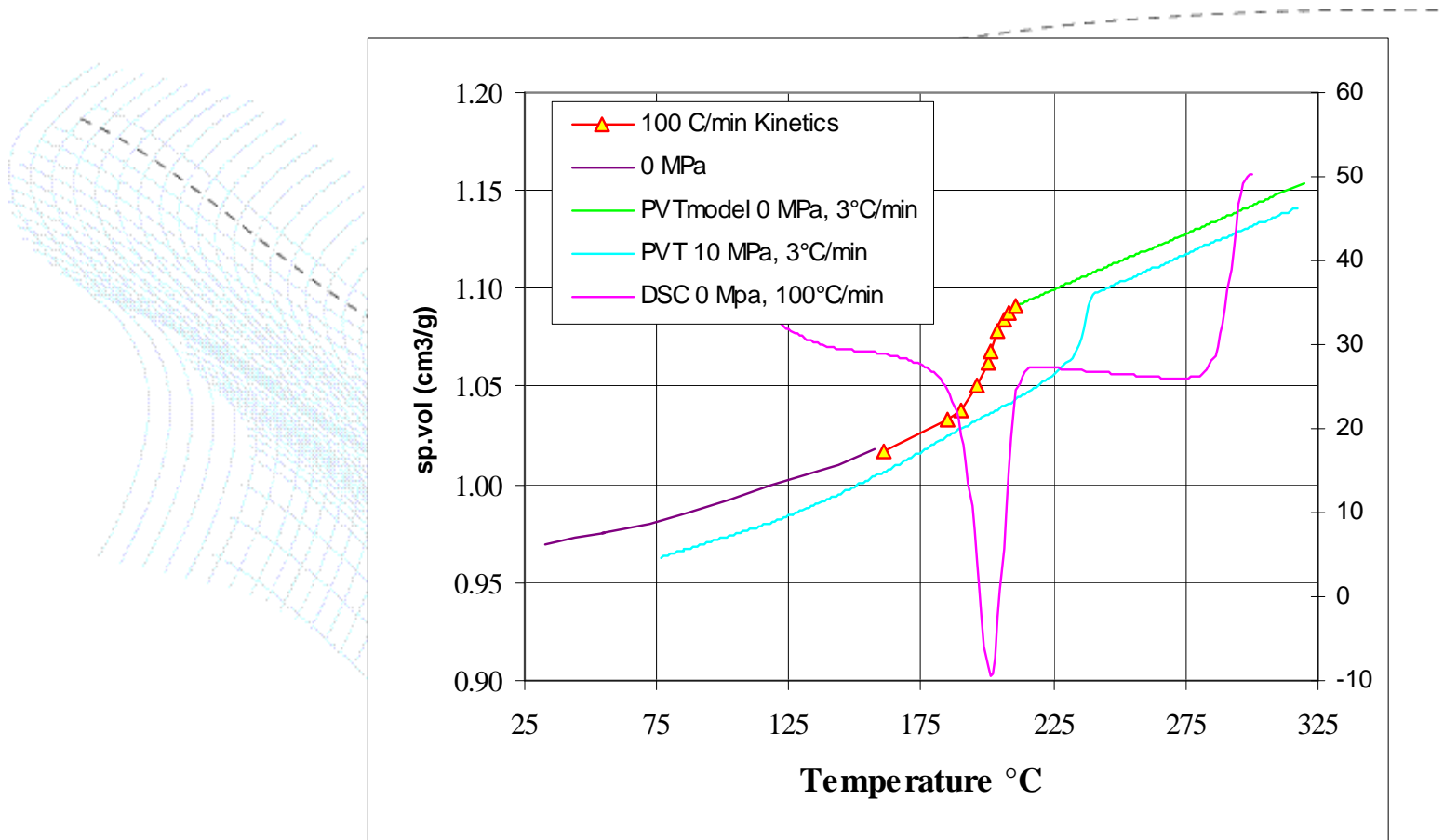
The PVT controversy

- C-MOLD- process is in cooling-
measure PVT in cooling
- Moldflow- Measure PVT while
heating

The PVT controversy- Realities



Accounting for rate with DSC



Lobo, Gordon Conference 98, Antec 99

TestPaks.com

matereality



DatapointLabs

Limitations

- Good for quiescent situations
- Supercooling effect overpredicted when there is flow
 - u Transition is closer to heating transition when shear effects present

What about high-rate PVT

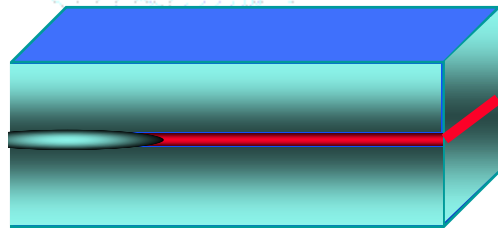
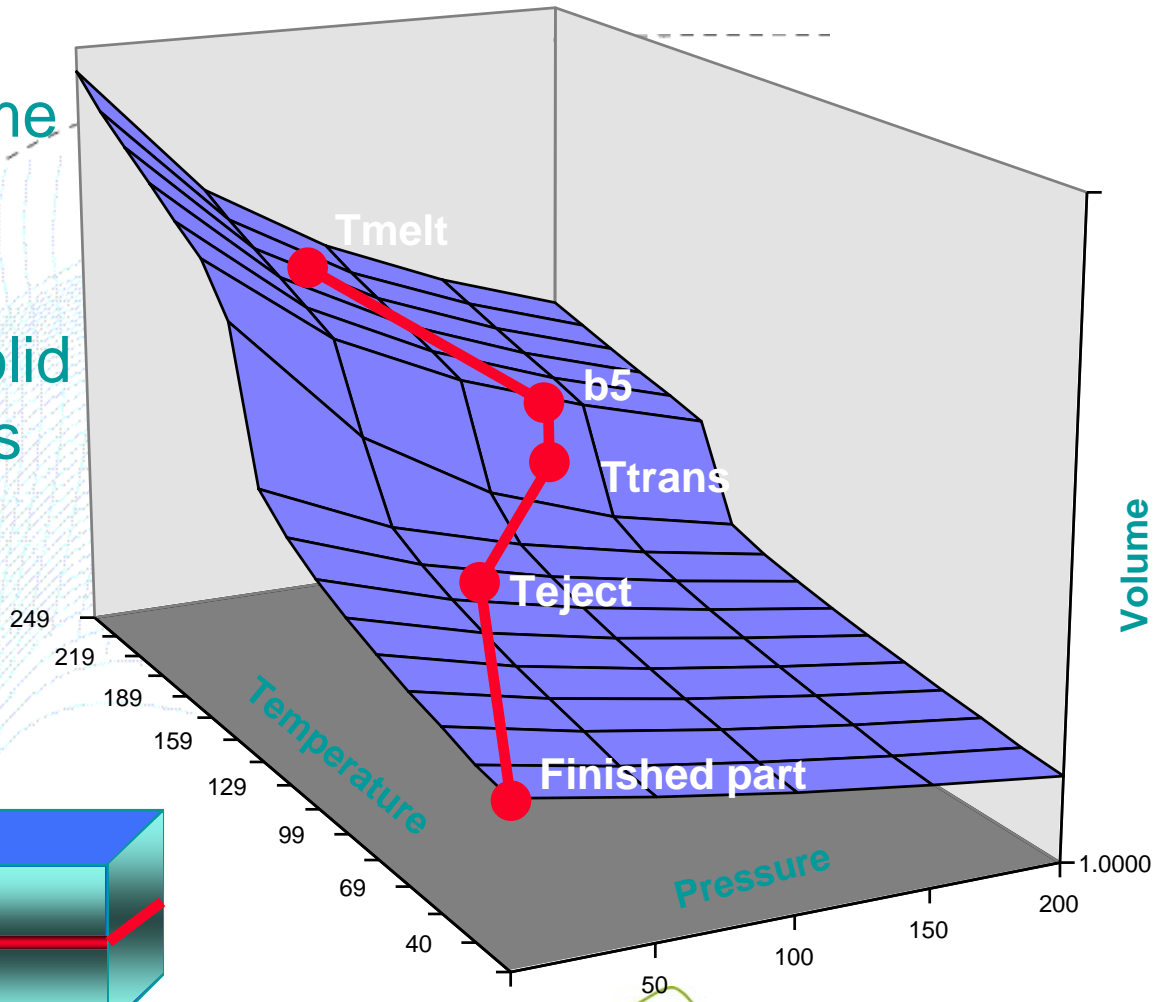
- Solid state data in PVT cooling will always be wrong
 - u No instrument can reproduce the unique frozen layer morphology or shear state of the injection molding process

Current Compromise

- Use PVT heating data
 - u Reasonable transition location
 - u Good representation of solid state PVT behavior

Shrinkage in simulation

- Change in volume in PVT data on cooling
- Starts at melt-solid transition- T_{trans}



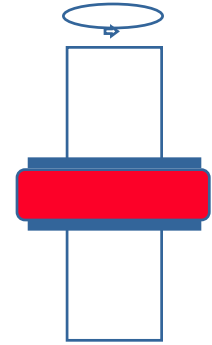
Consequences

- Small changes in T_{trans} = large change in shrinkage
- Must be grounded in PVT data of an injection-molded part

Melt-Solid transition

- DSC based methods
 - u Easy to get high cooling rates
 - u Quiescent material
- Shown to be not-representative
 - u Transitions are shear rate dependent

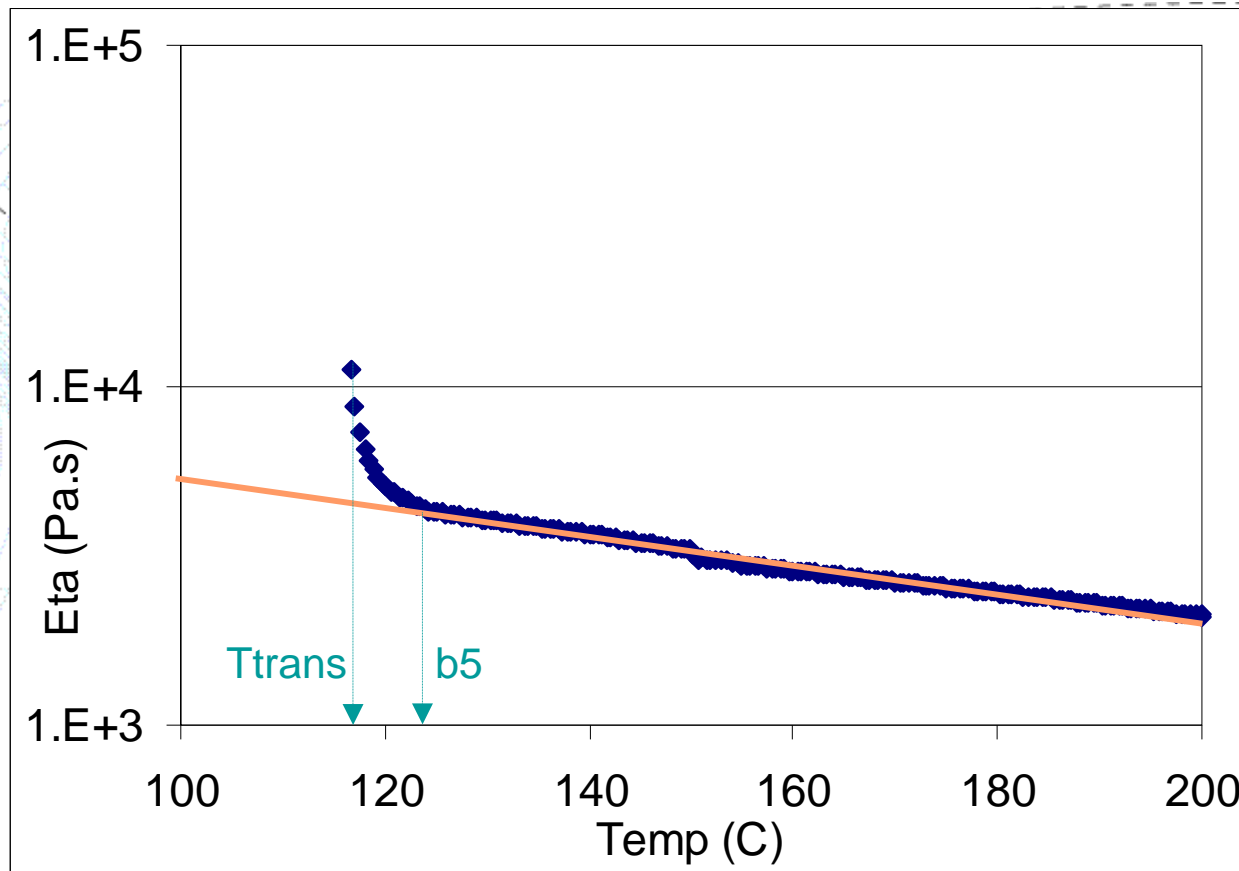
Melt-Solid transition



- DMA based methods
- High shear rate can be applied
- Slower cooling rates
- Also measures temp sensitivity of viscosity
- Set Ttrans based on modulus-material too stiff to flow

(See Lobo MUG2000)

DMA for Semi-crystalline plastic



Unified Material Model

- Capillary Viscosity at Process temp
- DMA cooling experiment at slow rate high frequency
 - u Ttrans, b5
 - u Temp sensitivity of viscosity (D1, D2)
- PVT in heating at same slow rate
- Thermal conductivity and specific heat transitions shifted to Ttrans